

BLASTING PERFORMANCE OPTIMIZATION AND COST REDUCTION

Pattern Expansion Optimization Model based on Fragmentation Analysis with Drone Technology

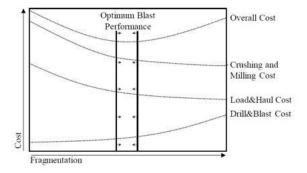
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As the mining industry faces growing pressure to find efficiencies, mining operations seek continuous improvement tools to validate their blasting procedures. Combining various technologies and solutions that consider terrain parameters, rock quality, and explosive strength to propose a practical method for pattern expansion that improves blasting processes has become a necessity.

CHALLENGE

Optimizing blasting performance to minimize costs and improve profitability in mining operations.

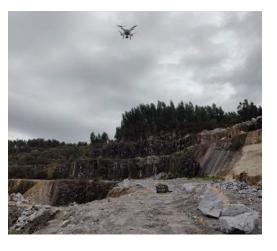
Mining operation costs are defined by crushing and milling, load and haul, and drilling and blasting charges. As drilling and blasting is the initial phase of mining operations, it dramatically affects the overall cost. Consequently, one primary challenge is optimizing blasting performance to achieve desired outcomes at the lowest possible price.





on model

gmentation



osts via technology-driven blast fragmentation analysis and optimization.

ng drill blast costs for the client we applied this solution. First, predicting pn-site issues. We used O-PitSurface, a blast design software, to support the ion and estimate optimal design parameters.

a drone flight to define the area to be analyzed, including ground sampling camera angle. The resulting photos were processed using photogrammetry orthophoto. We then analyzed the orthophoto in WipFrag resulting in a listribution data.

barameters, it was essential to have an accurate prediction model, such as the G non-linear programming optimization methodology in calibration to obtain measured fragmentations.





WipFrag iOS Solution

WipFrag iOS Particle size identification



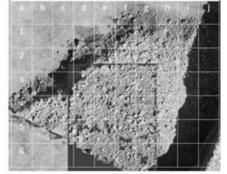


Figure 2. Fragmentation Analysis using WipFrag w/GIS



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| ROCK FACTOR CALIBRATION PROCESS | | | | | | | | |
|---------------------------------|-------------------|-----------------------|-----------------------|-----------------------|--|--|--|--|
| | Initial Parameter | Rock Factor Cal. STG1 | Rock Factor Cal. STG2 | Rock Factor Cal. STG3 | | | | |
| Diameter | 102 mm | 102 mm | 102 mm | 102 mm | | | | |
| Bench Height | 10 mm | 10 mm | 10 mm | 10 mm | | | | |
| Burden | 3,0 m | 3,0 m | 3,0 m | 3,0 m | | | | |
| Spacing | 3,5 m | 3,5 m | 3,5 m | 3,5 m | | | | |
| Subdrilling | 1,2 m | 1,2 m | 1,2 m | 1,2 m | | | | |
| Stemming | 2,8 m | 2,8 m | 2,8 m | 2,8 m | | | | |
| (KR Adjustes) X20 | 91 mm | 97 mm | 102 mm | 106 mm | | | | |
| (KR Adjustes) X50 | 190 mm | 204 mm | 213 mm | 224 mm | | | | |
| (KR Adjustes) X80 | 330 mm | 353 mm | 369 mm | 390 mm | | | | |
| (KR Adjustes) X90 | 416 mm | 446 mm | 446 mm | 493 mm | | | | |
| (Photo-Analysis) X20 | 190,9 mm | 114 mm | 117,8 mm | 115,3 mm | | | | |
| (Photo-Analysis) X50 | 209,6 mm | 220,7 mm | 225,8 mm | 235,9 mm | | | | |
| (Photo-Analysis) X80 | 347,7 mm | 364,5 mm | 384,1 mm | 399,5 mm | | | | |
| (Photo-Analysis) X90 | 433,7 mm | 457,1 mm | 480,7 mm | 506,1 mm | | | | |
| Rock Factor Cal. | 7 | 7,5 | 7,83 | 8,14 | | | | |

To obtain optimum blast design parameters, we defined a non-linear problem, including dependent variables, empirical restrictions, and fragmentation demands. We applied controllable changes at each improvement stage in the pattern expansion field to avoid excessive deviations.

We implemented a detailed fragmentation analysis to control blast results and expanded the pattern until the fragmentation limit was reached.

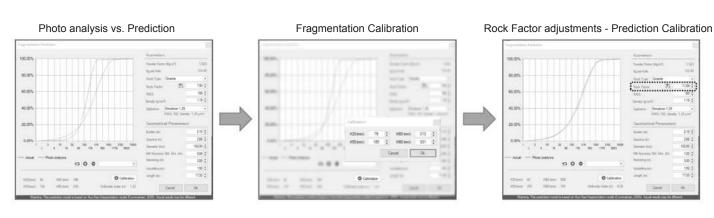


Figure 3. Rock Factor Calibration Process (O-Pitblast system)



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| Initial Stage | | | | | | Final Optimized Stage | | | | | | | | |
|---------------------------|-----------------|-------------------------|-------------------------|-----------------|-------------|-----------------------|-------------------------|---------------------------|------------------|-------------------------|--------------------|------------------|-------------|-----------------------|
| Optimization | | | | | | | | Optimization | | | | | | 1 |
| Geometry: | | Blast: | | Costs: | | | Dependent Variables | Geometry: | | Blast: | | Costs: | | |
| Diameter (mm): | 102 🗘 | Number of Holes: | 120 🌲 | Initiation (pe | er hole): | 10.00 🜲 | | Diameter (mm): | 102 🌩 | Number of Holes: | 85 🜩 | Initiation (pe | r hole): | 10.00 🜲 |
| Bench High (m): | 11.70 🜩 | Number of Rows: | 7 🜲 | Explosive (p | ber Kg): | 4.00 ≑ | | Bench High (m): | 11.70 🌻 | Number of Rows: | 7 🔹 | Explosive (p | er Kg): | 4.00 🜲 |
| Burden (m): | 3.70 🛟 | Volume (m³): | 15,623 🜲 | Drilling (per | meter): | 7.00 🌻 | | Burden (m): | 3.46 ≑ | Volume (m³): | 16,623 🗘 | Drilling (per r | meter): | 7.00 🌻 |
| Spacing (m): | 3.70 🗘 | | | | | | | Spacing (m): | 4.84 🌻 | | | | | |
| Subdrilling (m): | 1.10 🜲 | Geology: | | Explosive | B: | | | Subdrilling (m): | 1.66 🌻 | Geology: | | Explosive: | | |
| Stemming (m): | 3.10 🜲 | Rock Factor: | 10.00 🌲 | Density (g/o | cm³): | 1.20 🌲 | | Stemming (m): | 2.42 🛟 | Rock Factor: | 10.00 🌲 | Density (g/c | m³): | 1.20 🌻 |
| ragmentation: | | Constraints: | | RWS: | | 100 🌻 | Variable Constrainte | Fragmentation: | | Constraints: | | RWS: | | 100 🔹 |
| Limit (%): | 80 🗘 | Spacing by Burden | 1.00 🌲 | ≤ 1.00 | < | 1.40 🤤 ✔ | Conductine | Limit (%): | 85 🗘 | Spacing by Burden | 1.00 🌲 | ≤ 1.40 | ≤ | 1.40 🌻 ✔ |
| Oversize (mm): | 700 🗘 | Stemming by Burden | 0.70 🜲 | ≤ 0.84 | < | 1.00 💠 ✔ | | Oversize (mm): | 700 🛟 | Stemming by Burden | 0.70 🜲 | ≤ 0.70 | < | 1.00 🗘 🗸 |
| Information: | | Subdrilling by Burden | 0.30 🌻 | ≤ 0.30 | < | 0.50 🤤 🗸 | | Information: | | Subdrilling by Burden | 0.30 🜩 | ≤ 0.48 | < | 0.50 🗘 🗸 |
| information. | | Uniformity Index | 0.70 🜲 | ≤ 1.35 | ≤ | 2.20 🗘 🗸 | | | | Uniformity Index | 0.70 🜲 | ≤ 1.70 | ≤ | 2.20 🗘 🗸 |
| Powder Factor (Kg/m³): | 0.594 | Stiffness Ratio | | 3.16 | 2 | 3.00 🗘 🗸 | Objective | Powder Factor (Kg/m³): | 0.547 | Stiffness Ratio | | 3.38 | 2 | 3.00 🗘 🗸 |
| Specific Drilling (m/m³): | 0.0799 | Volume (m³): | | 19220.76 | ≥ 15623 | ✓ | Variable | Specific Drilling (m/m³): | 0.0682 | Volume (m³): | | 16654.29 | ≥ 1662 | з 🗸 |
| | | Oversize (mm): | | 660.97 | ≤ 700 | ~ | Vanabio | | | Oversize (mm): | | 697.23 | ≤ 700 | ✓ |
| | | | | Cost (\$): | 9 | \$57,606.59 | Fi | ind Optimized Va | lues | | | Cost (\$): | | \$45,271.88 |
| Find optmized va | lues 🟮 | Apply Pattern 上 G | iet Values om Design | | | Ok | | Find optmized val | ues 🖸 | Apply Pattern | alues am Design | | [| Ok |
| Warning: This pre | diction model i | s based on GRG Nonlinea | r optimization mo | del. Actual res | ults may be | different. | | Warning; This pred | diction model is | s based on GRG Nonlinea | r optimization mo | del. Actual resi | ults may be | e different. |

RESULTS

Integrating technology in daily mining tasks is crucial in enhancing safety and production efficiency. The initial design parameters are presented in the Table below for the present study.

| INITIAL BLAST DESIGN PARAMENTERS | | | | | | |
|----------------------------------|------------|--|--|--|--|--|
| Burden | 3,0 m | | | | | |
| Spacing | 3,5 m | | | | | |
| Diameter | 102 mm | | | | | |
| Stemming | 2,8 mm | | | | | |
| Subdrill | 1,2 m | | | | | |
| Bench Height | 10 m | | | | | |
| Powder Factor | 0,77 kg/m³ | | | | | |

The idea behind the pattern expansion field is to avoid excessive deviations simultaneously. Controllable changes were applied at any improvement stage and detailed fragmentation analyses were performed to control the blast results. The pattern was expanded until the fragmentation limit was reached. In the Table below, it is possible to check the evolution of each stage in terms of changes and results.







| PATTERN EXPANSION EVOLUTIONARY STAGES | | | | | | | | | |
|---------------------------------------|---------------|----------|----------|----------|----------|---------|--|--|--|
| | Initial Stage | Stage 1 | Stage 2 | Stage 3 | Stage 4 | Stage 5 | | | |
| Diameter | 102 mm | 102 mm | 102 mm | 102 mm | 102 mm | 102 mm | | | |
| Bench Height | 10 mm | 10 mm | 10 mm | 10 mm | 10 mm | 10 mm | | | |
| Burden | 3,0 m | 3,1 m | 3,1 m | 3,2 m | 3,3 m | 3,3 m | | | |
| Spacing | 3,5 m | 3,6 m | 3,7 m | 3,8 m | 3,9 m | 4,0 m | | | |
| Subdrilling | 1,2 m | 1,2 m | 1,1 m | 1,1 m | 1,0 m | 1,0 m | | | |
| Stemming | 2,8 m | 2,9 m | 3,0 m | 3,1 m | 3,2 m | 3,3 m | | | |
| (KR Adjustes) X20 | 105 mm | 109 mm | 113 mm | 117 mm | 121cmm | 125 mm | | | |
| (KR Adjustes) X50 | 221 mm | 233 mm | 245 mm | 257 mm | 270 mm | 283 mm | | | |
| (KR Adjustes) X80 | 383 mm | 409 mm | 433 mm | 461 mm | 488 mm | 520 mm | | | |
| (KR Adjustes) X90 | 484 mm | 519 mm | 552 mm | 591 mm | 629 mm | 689 mm | | | |
| (Photo-Analysis) X20 | 124,5 mm | 134,7 mm | 151,8 mm | 171,2 mm | 223,9 mm | N/A | | | |
| (Photo-Analysis) X50 | 240,1 mm | 275,8 mm | 303,4 mm | 327,1 mm | 352,6 mm | N/A | | | |
| (Photo-Analysis) X80 | 398,1 mm | 449,9 mm | 480,3 mm | 517,8 mm | 543,1mm | N/A | | | |
| (Photo-Analysis) X90 | 501,5 mm | 541,9 mm | 604,4 mm | 653,8 mm | 714,8 mm | N/A | | | |

In summary, using O-Pitblast's blast optimization algorithm, the client reduced costs by 229,361 and blasted through 605,307 m³/791,712 yd³ of rock.

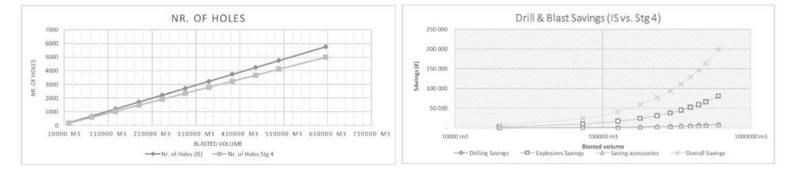




Figure 5. Drill and Blast Savings



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ABOUT US

At O-Pitblast, we aim to humanize mining by positively impacting every aspect of the blasting process.

As a leading provider of innovative blasting solutions, we prioritize people, ensuring the safety and well-being of our teams, communities, and the environment.

With a proven track record in providing tailored blasting solutions, O-Pitblast is the preferred partner for the global mining industry.

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- O Global reach with solutions on multiple continents.
- O Cutting-edge software and hardware for blast design.
- O Commitment to environmentally friendly practices
- > Highly qualified and dedicated support team.
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